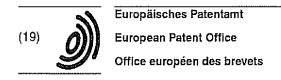
Polytetrafluoroethylene agglomerated product and its molded product

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Abstract of EP 1213321 (A2)

A polytetrafluoroethylene agglomerated product obtained from a polytetrafluoroethylene powder and a coke powder, wherein the polytetrafluoroethylene powder contains at least 8.3 mass% of a polytetrafluoroethylene fine powder having a particle diameter of from 0.1 to 9 5 mu m, and the mass ratio of the polytetrafluoroethylene powder/the coke powder is 95-60/5-40

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(54) Polytetrafluoroethylene agglomerated product and its molded product

(57) A polytetrafluoroethylene agglomerated product obtained from a polytetrafluoroethylene powder and a coke powder, wherein the polytetrafluoroethylene powder contains at least 8 3 mass% of a polytetrafluoroethylene fine powder having a particle diameter of from 0.1 to 9.5 μ m, and the mass ratio of the polytetrafluor-oethylene powder/the coke powder is 95-60/5-40.

Description

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[0001] The present invention relates to a tetrafluoroethylene agglomerated product which is useful as a molding material for e.g. sliding members

[0002] Polytetrafluoroethylene (hereinafter referred to as PTFE) produced by suspension polymerization is used for molding by compression molding or ram extrusion molding. By suspension polymerization, PTFE particles having an average particle diameter of from 2 to 5 mm are usually obtained, and such particles are pulverized and used for various applications in the form of a PTFE powder having an average particle diameter of from 25 to 65 µm

Particularly, a PTFE agglomerated product obtained by uniformly mixing a PTFE powder having an average particle diameter of from 25 to 65 μ m with various fillers to obtain a composition, followed by agglomeration, is used as a powder for molding

[0003] A molded product obtained by molding such a PTFE agglomerated product has physical properties such as abrasion resistance and hardness improved over a molded product of PTFE containing no filler, and is widely used as various sliding members for sealing. However, in a case of producing a thin molded product or a very small molded product, such a PTFE agglomerated product has no adequate property such as powder flow properties required for automated filling into a mold for molding.

[0004] JP-A-7-11088 discloses a PTFE agglomerated product obtained from a PTFE powder having an average particle diameter of at most 20 µm and a filler. It is disclosed that a PTFE agglomerated product obtained by using a glass fiber powder, a graphite powder, a bronze powder, a carbon fiber powder, etc., as a filler, has excellent powder flow properties and a high bulk density and is useful for automation of the molding process by a mold or for improvement of the productivity. However, with respect to use of a coke powder as a filler, there is no disclosure

[0005] Recently, a sliding member such as a so-called non-cut seal ring to be fit on a slide shaft while elongating the seal ring by means of a jig, is used in various apparatus. Accordingly, a sliding member having high elongation, which is useful for application to such a seal ring, is required, and the demand for a PTFE molded product having high elongation is increasing. Particularly, a sliding member having a high hardness excellent in abrasion resistance in addition to the high elongation is required for a seal ring on a sliding surface of an apparatus made of a material of high hardness such as iron or stainless steel.

[0006] JP-B-8-30135 discloses a composition comprising a graphite powder and a PTFE powder A molded product obtained by molding this composition has high elongation, but the hardness is low Further, such a composition is inadequate in the powder flow properties at the time of molding. Further, with respect to a PTFE agglomerated product, there is no disclosure.

[0007] JP-A-11-21407 discloses a composition comprising PTFE and a carbon filler having a specific surface area of at most 3 m²/g. A molded product obtained by molding such a composition has high elongation, but such a composition is inadequate in the powder flow properties. Further, with respect to a PTFE agglomerated product, there is no disclosure.

[0008] It is an object of the present invention to provide a PTFE agglomerated product having excellent powder flow properties and a high bulk density, and a molded product having high elongation and high hardness, obtained by molding such a PTFE agglomerated product

[0009] The present invention provides a polytetrafluoroethylene agglomerated product obtained from a polytetrafluoroethylene powder and a coke powder, wherein the polytetrafluoroethylene powder contains at least 8 3 mass% of a polytetrafluoroethylene fine powder having a particle diameter of from 0.1 to 9.5 μ m, and the mass ratio of the polytetrafluoroethylene powder/the coke powder is 95-60/5-40

[0010] Further, the present invention provides a molded product obtained by molding such a PTFE agglomerated product

[0011] Now, the present invention will be described in detail with reference to the preferred embodiments

[0012] The PTFE powder in the present invention contains at least 8.3 mass% of a PTFE fine powder having a particle diameter of from 0.1 to 9.5 µm (hereinafter referred to simply as the PTFE fine powder). If the content of the PTFE fine powder (hereinafter referred to as the PTFE fine powder content) in the PTFE powder is less than 8.3 mass%, the agglomerative tendency at the time of the production of the agglomerated product tends to be low, the powder flow properties of the PTFE agglomerated product thereby obtained, tends to be poor, and the elongation of the molded product tends to be low. The PTFE fine powder content in the PTFE powder is preferably at least 10 mass%, more preferably at least 12 mass%.

[0013] Further, the smaller the particle diameter of the PTFE fine powder, the better the agglomerative tendency However, if the particle diameter is too small, production of such a PTFE fine powder tends to be difficult. On the other hand, with a PTFE fine powder having a particle diameter exceeding 9.5 μ m, the effect for improvement of the agglomerative tendency is not large enough. If PTFE particles having too large particle diameters are contained in the PTFE powder, the agglomerative tendency tends to be low, the powder flow properties of the agglomerated product tends to be low, and a molded product having a high elongation tends to be hardly obtainable. The maximum particle diameter

of the PTFE powder is preferably at most 750 μm, more preferably at most 600 μm, most preferably at most 450 μm [0014] As a method for producing the PTFE powder in the present invention, it is preferred to pulverize PTFE particles having an average particle diameter of from 2 to 5 mm obtained by suspension polymerization. Particularly, a PTFE powder having an average particle diameter of at most 20 μm is preferred. For example, a PTFE powder having an average particle diameter of 20 μm obtained by pulverization contains 15 mass% of a PTFE fine powder.

[0015] Further, as a method for producing the PTFE powder in the present invention, it is also preferred to mix the PTFE powder having an average particle diameter of at most 20 μ m, obtained by the pulverization, with a PTFE powder having an average particle diameter of from 25 to 65 μ m, which is readily available. For example, when a PTFE powder having an average particle diameter of 5 7 μ m and having a PTFE fine powder content of 90 mass% and a PTFE powder having an average particle diameter of 35 1 μ m and having a PTFE fine powder content of 8 mass% are mixed by means of a Henschel mixer in a mass ratio of 20/80, a PTFE powder having an average particle diameter of 32 9 μ m and having a PTFE fine powder content of 11 7 mass%, can be obtained

[0016] As PTFE, a homopolymer of tetrafluoroethylene (hereinafter referred to as TFE) is employed, but PTFE containing polymerized units based on a comonomer copolymerizable with TFE in a proportion of at most 0.5 mol%, which will not impart melt flow properties, may also be employed

[0017] Specific examples of such a comonomer may be fluoroolefins other than TFE, such as hexafluoropropylene, chlorotrifluoroethylene and trifluoroethylene, fluorovinyl ethers such as a perfluoro(alkyl vinyl ether), a perfluoro(alkoxy alkyl vinyl ether) and a (perfluoroalkyl) methyl trifluorovinyl ether, and olefins such as a (perfluoroalkyl)ethylene, ethylene and propylene Particularly preferred are hexafluoropropylene, perfluoro(n-propyl vinyl ether) and (perfluoro-n-butyl)ethylene.

[0018] In the present invention, the average particle diameter of the coke powder is preferably from 1 to 50 μm . If the average particle diameter of the coke powder is too small, elongation of the PTFE molded product will be low, and if it is too large, the abrasion resistance of the PTFE molded product will be low. More preferably, the average particle diameter of the coke powder is from 10 to 35 μm

[0019] In the present invention, the mass ratio of the PTFE powder/the coke powder is 95-60/5-40. If the PTFE powder is too much, the hardness of the molded product will be inadequate, and if it is too small, the tensile strength and elongation of the molded product tends to be low. The mass ratio of the PTFE powder/the coke powder is preferably 90-65/10-35. Especially, in order to obtain a molded product having a high hardness, the mass ratio of the PTFE powder/the coke powder is more preferably 85-65/15-35.

[0020] As a method for producing the PTFE agglomerated product of the present invention, it is possible to employ a dry method wherein no water is used, or a wet method wherein water is used. In the dry method, it is preferred that the PTFE powder and the coke powder, as the starting materials, are mixed by e.g. a Henschel mixer, and then, an organic solvent is added thereto as a binder, followed by agglomeration by a agglomeration machine of tumbling type, agitation type or fluidized bed type. In the wet method, it is preferred that using an organic medium insoluble in water as a binder, a mixture of the PTFE powder and the coke powder as the starting materials, is stirred in water for agglomeration.

[0021] In the present invention, the functional mechanism of the PTFE powder and the coke powder is not necessarily clearly understood, but is considered to be as follows. By the use of the PTFE powder having a high PTFE fine powder content, the adhesive forces among the PTFE powder and between the PTFE powder and the coke powder are increased, and the agglomerative tendency is thereby improved, whereby a PTFE agglomerated product which is dense and has a high bulk density and which is excellent in the powder flow properties, can be obtained. Further, it is considered that by the combination of the coke powder to such a PTFE powder, a PTFE molded product having high elongation and high hardness, can be obtained.

[0022] As the method for molding the PTFE agglomerated product of the present invention, a compression molding method or a ram extrusion molding method may, for example, be employed in the compression molding method, the following molding conditions are preferred. Molding pressure at the time of preforming: 44 to 118 MPa; molding speed: 100 mm/min until 1/2 of the stroke length is reached, and 20 mm/min after 1/2 of the stroke length is reached, until the maximum pressure; holding time at the maximum pressure: 2 minutes per kg of the powder; the maximum sintering temperature at the time of sintering: 360 to 380°C; holding time at the maximum temperature: time X calculated by the following formula; temperature raising and cooling rate: 50 to 70°C/hr

X = 2 + (wall thickness (unit: cm) of the molded

product) × (1 hr/1 cm of wall thickness)

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[0024] Now, the present invention will be described in further detail with reference to Examples (Examples 1 to 4, 9 and 10) and Comparative Examples (Examples 5 to 8 and 11) However, it should be understood that the present invention is by no means restricted to such specific Examples. The properties of the PTFE powder and the PTFE agglomerated product were measured by the following methods

Particle diameters (unit: µm) of the PTFE powder and the coke powder

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[0025] Measured by laser diffraction type particle diameter distribution measuring apparatus SALD-3000, manufactured by Shimadzu Corporation. From the obtained particle diameter distribution of the PTFE powder, the PTFE fine powder content and the average particle diameter of the PTFE powder were calculated by integral calculus

Average particle diameter (unit: µm) of the PTFE agglomerated product

[0026] Sequentially from the top, standard sieves of 10, 20, 35, 40 and 60 mesh, were put together, and the PTFE agglomerated product was placed on the 10 mesh sieve, followed by shaking, whereupon the mass of the PTFE agglomerated product remaining on each sieve, was obtained Based on this mass, the 50% particle diameter was obtained by a logarithmic probability paper and was taken as the average particle diameter of the PTFE agglomerated product

Bulk density (unit: g/ℓ) of the PTFE agglomerated product

[0027] Measured in accordance with JIS K6891 Into a stainless steel weighing bottle having an internal volume of 100 m ℓ , a sample of the PTFE agglomerated product was dropped from a funnel set above, and the sample bulging from the weighing bottle was scraped off with a flat plate, whereupon the weight of the sample remaining in the bottle was measured, and a value obtained by dividing the measured weight by the internal volume of the weighing bottle, was taken as the bulk density

Powder flow properties (unit: mm) of the PTFE agglomerated product

[0028] 100g of a sample of the PTFE agglomerated product was put into a container having a hopper shape, and the bottom of the container was opened at a constant rate, whereby the distance of the opening (the slit) when about 50g of the sample was dropped, was taken as the powder flow properties. The smaller the numerical value, the better the powder flow properties.

35 Tensile strength (unit: MPa) and elongation (unit: %)

[0029] Measured in accordance with JIS K6891. A test sample was prepared as follows. The PTFE agglomerated product was preformed under a pressure of 58.9 MPa and baked at 370°C for 4 hours, followed by cooling at a temperature lowering rate of 70°C/hr to obtain a sheet having a thickness of 2 mm, from which a test sample was punched out by a dumbbell No. 3 die. However, in Example 6, instead of the PTFE agglomerated product, a test sample obtained by molding a PTFE composition, was used.

Hardness (unit: durometer D)

45 [0030] Measured in accordance with JIS K7215.

EXAMPLES 1 to 5

[0031] PTFE powders as identified in Table 1 (FLUON G190 series, manufactured by ASAHI GLASS FLUOROPOLYMERS CO, LTD) were used. When PTFE powders were used as mixed, a Henschel mixer was used. For example, in Example 3, FLUON G190-5 and FLUON G190-35 were mixed in a mass ratio of 50/50 by a Henschel mixer at a peripheral speed of stirring vanes of 40 m/sec for a stirring time of 90 seconds, to obtain a PTFE powder. The obtained PTFE powder contained 24.1 mass% of a PTFE fine powder and had an average particle diameter of 25.5 µm. Also in Example 4, a PTFE powder obtained by preliminary mixing in the same manner as in Example 3, was used. The PTFE fine powder contents in the obtained PTFE powders were measured, and the results are shown in Table 2.

Table 1

Fluon No	Average particle diameter (μm)	PTFE fine powder content (mass%)	Maximum particle size (μm)
G190-5	5 7	90 0	25.6
G190-10	11 9	32 4	69 0
G190-35	35 1	8 1	336 4
G163-35	40 0	52	442 0

[0032] To 800g of the PTFE powder, 200g of a coke powder having an average particle diameter of 30 µm (KC-200, manufactured by Fuji Kokuen K K) was added, followed by mixing by a Henschel mixer at a peripheral velocity of stirring vanes of 40 m/sec for a stirring time of 90 seconds, to obtain a PTFE composition. The obtained PTFE composition was agglomerated by using petroleum naphtha as a binder, and the particle diameter was adjusted by a pan pelletizer, followed by drying to obtain a PTFE agglomerated product. In Table 2, the mixing mass ratio of the PTFE powder and the coke powder as the starting materials, the average particle diameter, bulk density and powder flow properties of the obtained PTFE agglomerated product, and the tensile strength, elongation and hardness of the molded product obtained by molding the PTFE agglomerated product, are shown

EXAMPLE 6

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[0033] The starting materials as identified in Table 2 were mixed by a Henschel mixer at a peripheral speed of stirring vanes of 40 m/sec for a stirring time of 90 seconds to obtain a PTFE composition. The bulk density and powder flow properties of the obtained PTFE composition were measured in the same manner as the PTFE agglomerate product. Further, the properties of a molded product of the PTFE composition obtained by molding in the same manner as the PTFE agglomerated product, were measured in the same manner as in Examples 1 to 5, and the results are shown in Table 2.

EXAMPLES 7 and 8

[0034] A PTFE agglomerated product and a molded product were obtained in the same manner as in Examples 1 to 4 except that 200g of a graphite powder having an average particle diameter of 30 μ m (KS-75, manufactured by Fuji Kokuen K K) was used instead of the coke powder. The properties of the PTFE agglomerated product and the properties of the molded product were measured in the same manner as in Examples 1 to 4, and the results are shown in Table 2.

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Table 2		WEATHER THOUSAND TO THE TOTAL TOTAL TO THE THE TOTAL TO T	V140400							
			Ex. 1	Ex. 2	Ex. 3	Ex. 4	EX.	Ex. 6	Ex. 7	Ex. 8
		G190-5	80		40	20	ł	_	80	1
	PTFE	G190-10	1	80	ſ	I	1	1	I	ŀ
Starting	powder	powder G190-35	#	ļ	40	60	80	80	•	80
material		G163-35	1	ţ	_	ı	1	1		, t
composition	Coke powder	Jwder	20	20	20	20	20	20	,	1
	Graphi	Graphite powder	ŧ	1	ı	1	_	Ī	20	20
PTFE fine pow	powder content	tent	90.06	32.4	24.1	11.7	8.1	8.1	0.06	8.1
Properties	Bulk density	ənsity		1	-	1	-	516	ļ	ŧ
of the	ņ				THE STATE OF THE S			L		
composítion	rowder.	FOWGER TOW DIODELLIES	1	ı	1	1	1	33	į	1
Properties	Average	e particle diameter	570	520	845	490	475	ı	460	465
of the	Bulk density	ensity	768	765	761	710	755	1	722	692
agglomerated	ار ار ار	() () () () () () () () () ()	Ç	Ċ	**	0			ŗ	ti r
product	で	rowder trow properties	7	7	1	0	n .	ı	77	CT
Properties	Tensile	e strength	16.3	16.0	15.1	18.6	14.4	21.3	13.9	11.9
of the	Elongation	inon	325	275	255	324	205	333	288	127
molded	; ; ;		ŗ	ŗ	C	(Ç	······································	Ç L	C L
product	Hardness	so,	63	63	63	00	0.3	ı	Ų.	ע ע

EXAMPLES 9 to 11

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[0035] With the starting material composition as identified in Table 3, a PTFE agglomerated product was obtained in the same manner as in Examples 1 to 5. The average particle diameter, bulk density and powder flow properties of the obtained PTFE agglomerated product, and the tensile strength, elongation and hardness of a molded product obtained by molding the PTFE agglomerated product, are shown in Table 3.

Table 3

			Ex 9	Ex 10	Ex 11
Starting material composition	PTFE powder	G190-5	20	35	_
		G190-10	,	-	
		G190-35		w	-
		G163-35	50	35	35 -
	Coke powder		30	30	30
	Graphite powde	er			-
PTFE fine powder content			8 4	22 0	5.2
Properties of the composition	Bulk density		-	-	-
	Powder flow properties		-	_	-
Properties of the agglomerated product	Average particle diameter		490	450	510
	Bulk density		686	680	620
	Powder flow properties		11	25	32
Properties of the molded product	Tensile strength		147	16 9	148
	Elongation		62	68	45
	Hardness		70	72	70

[0036] The PTFE agglomerated product of the present invention has a high bulk density and is excellent in the powder flow properties, and thus, it is useful for e.g. automation of the molding process by a mold or improvement of the productivity. Further, the molded product obtained from the PTFE agglomerated product of the present invention has high elongation and high hardness, and thus, it is useful as a sliding member such as a sealing ring to be stretched and mounted on a sliding surface having high hardness.

[0037] The entire disclosures of Japanese Patent Application No. 2000-370588 filed on December 5, 2000 and Japanese Patent Application No. 2001-278064 filed on September 13, 2001 including specifications, claims and summaries are incorporated herein by reference in their entireties

Claims

- A polytetrafluoroethylene agglomerated product obtained from a polytetrafluoroethylene powder and a coke powder, wherein the polytetrafluoroethylene powder contains at least 8 3 mass% of a polytetrafluoroethylene fine powder having a particle diameter of from 0.1 to 9.5 μm, and the mass ratio of the polytetrafluoroethylene powder/the coke powder is 95-60/5-40
- 50 2. The polytetrafluoroethylene agglomerated product according to Claim 1, wherein the polytetrafluoroethylene powder der contains at least 10 mass% of the polytetrafluoroethylene fine powder
 - The polytetrafluoroethylene agglomerated product according to Claim 1, wherein the polytetrafluoroethylene powder contains at least 12 mass% of the polytetrafluoroethylene fine powder
 - 4. The polytetrafluoroethylene agglomerated product according to any one of Claims 1 to 3, wherein the maximum particle diameter of the polytetrafluoroethylene powder is at most 450 μm

- 5. The polytetrafluoroethylene agglomerated product according to any one of Claims 1 to 4, wherein the average particle diameter of the coke powder is from 1 to 50 μm 6. The polytetrafluoroethylene agglomerated product according to any one of Claims 1 to 5, wherein the average particle diameter of the coke powder is from 10 to 35 µm. 7. The polytetrafluoroethylene agglomerated product according to any one of Claims 1 to 6, wherein the mass ratio
- of the polytetrafluoroethylene powder/the coke powder is 90-65/10-35

8. A molded product obtained by molding the agglomerated product as defined in any one of Claims 1 to 7

9. A molded product obtained by molding the agglomerated product as defined in any one of Claims 1 to 7 by com-

pression molding or ram extrusion molding 15 20 25 30

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